



Failure Process Modeling with Censored Data in Accelerated Life Tests

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ABSTRACT

Manufacturers need to evaluate the reliability of their products in order to increase the customer satisfaction. Proper analysis of reliability also requires an effective study of the failure process of a product, especially its failure time. So, the Failure Process Modeling (FPM) plays a key role in the reliability analysis of the system that has been less focused on. This paper introduces a framework defining an approach for the failure process modeling with censored data in Constant Stress Accelerated Life Tests (CSALTs). For the first time, various types of censoring schemes are considered in this study. Usually, in data analysis, it is impossible to get closed form of estimates of the unknown parameter due to complex and nonlinear likelihood equations. As a new approach, a mathematical programming problem is formed and the Maximum Likelihood Estimation (MLE) of parameters is obtained to maximize the likelihood function. A case study in red Light- Emitting Diode (LED) lamps is also presented. The MLE of parameters is obtained using genetic algorithm (GA). Furthermore, the Fisher information matrix is obtained for constructing the asymptotic variances and the approximate confidence intervals of estimates of the parameters.

KEYWORDS

Reliability; Failure process modeling; Accelerated life test; Censored data.

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1. INTRODUCTION

Reliability is one of the most important qualitative characteristics of the complex products. It measures the level of efficiency of systems. In recent years, many manufacturers have used reliability as an essential factor for improving the quality of their products and aimed at reducing the failures of costly components as a strategic policy, since inadequate reliability results in poor economic performance and extra costs for both the manufacturer and the customer. So, manufacturers need to evaluate the reliability of their products in order to increase the customer satisfaction. In order to improve the reliability of products, quantitative methods should be used to predict and analyze various aspects of reliability. Proper analysis of reliability also requires an effective study of the failure process of a product, especially its failure time. So the failure process modeling plays a key role in reliability analysis of the systems. Different frameworks have been suggested for the investigation of the FPM of systems in the literature; for example, see [1-4].

Lifetime experiments are performed on products to obtain their failure times. One of the important issues in reliability analysis is how to collect the lifetime data of the products in a limited time, as the mean time to failure of products might be very high under the normal operating conditions. So, in reliability and lifetime measurement experiments, test units are usually exposed to stress levels higher than normal operating conditions, leading to a shorter lifetime and accelerated damage. As a result, lifetime data required to determine unknown parameters is obtained faster than the normal operating conditions [5]. Consequently, components are affected by different types of stresses such as temperature, voltage, vibration, pressure, load, and humidity, which directly affect their lifetime. This type of testing is known as Accelerated Life Test (ALT). For the first time, Chernoff [6] and Bessler et al. [7] introduced the concept of accelerated life testing in 1962. Data obtained from these experiments are used to estimate the lifetime parameters such as Mean Time To Failure (MTTF) and reliability in normal operating conditions.

In general, ALTs can be classified into three categories: constant stress accelerated life test, Step Stress Accelerated Life Test (SSALT), and Continuously Increasing Stress Accelerated Life Test (CISALT). The basis for this classification is the time dependency of the stress variables. CSALT is the most common method. In this method, the stress applied to the units is time-independent and each unit runs at a constant stress level

until the test is terminated [8]. This method has been studied extensively by several authors. Bai and Chung [9] proposed CSALT models based on the Weibull lifetime distributions. Kolarik and Teng [10] designed and performed a CSALT on direct current motors. It involved on/off cycling vs. continuous operation under multiple stresses. They considered the voltage, load, and operation mode as the stress factors. The two-parameter Weibull distribution with a constant shape parameter was used for the failure data analysis. Fan and Yu [11] discussed the reliability analysis of the CSALTs when a parameter in the generalized Gamma lifetime distribution is linear in the stress level. Zhang et al. [12] predicted the life of White Organic Light Emitting Display (OLED) using CSALTs. Guan et al. [13] studied the optimal CSALTs with complete sample for the generalized Exponential distribution.

Usually in data analysis, it is impossible to get closed form of estimates of the unknown parameter due to the complex and nonlinear likelihood equations. In this paper, as a new approach, a mathematical programming problem was formed and the maximum likelihood estimation of parameters is obtained to maximize the likelihood function using optimization tools.

In order to be effective, reliability data set should contain both failure times and censored times. Therefore, lifetime data could be separated into two categories: complete or censored. Complete data means the failure time of each test unit is observed or known. Censoring is one of the most common ways in reliability analysis that plays an important role in FPM. This method is applied when some of the units in the sample do not fail during the test, or the exact failure times of all units are not known. In general, censoring is done based on the time of failures, their number, or a combination of both. There are different types of censoring schemes: left censoring, right censoring, interval censoring, random censoring, Type-I and Type-II censoring, Type-I and Type-II hybrid censoring, and progressive censoring [14].

CSALT have been studied under different types of censoring in the recent years. Yang [15] calculated the optimum plan of four-level CSALT with various censoring times. In this study, the optimum plan was chosen by the stress levels, test units allocated to each stress, and censoring times to minimize the asymptotic variance of the MLE of the mean (log) life at design stress and test length. Mettas [16] described a model for a typical three stress type CSALT data with censoring. The temperature, voltage, and operation type were considered to be the stress factors. The Weibull distribution with a

constant shape parameter was also used to analyze the failure data. Three scenarios were considered in the tests: (a) only the temperature effect, (b) temperature and voltage, and (c) all three stress variables. Zhou et al. [17] considered the geometric process implementation of the CSALT model based on the progressive Type-I hybrid censored data.

In previous studies, up to three types of censoring schemes which have been investigated; however, various types of censoring schemes have been considered in this study. A summary of the literature review based on type of ALT, type of censoring scheme, lifetime distribution, estimation method, and case study is presented in Table 1.

A correct definition of the model describing the failure process is a very important issue that has been less focused on. This paper presents a framework defining an approach for FPM with the censored data in CSALTs. For the first time, various types of censoring schemes have been considered in this study. As a new approach, mathematical programming tools were used for getting the maximum likelihood estimation of the unknown parameters with mathematical solving approach in data analysis phase. As a case study, the framework was used for the reliability analysis of red light-emitting diode lamps. This paper has been organized as follows: Description of FPM framework discusses the framework for the FPM. Case study presents a case study describing the reliability analysis of the red LED lamps. Finally, the conclusion outlines the conclusions and further research.

2. DESCRIPTION OF FAILURE PROCESS MODELING FRAMEWORK

This section provides a framework defining an approach for FPM with censored data in CSALTs from initial data collection to reliability parameter estimation. The aim of framework is to estimate the reliability under the normal operating conditions, which is achieved by FPM and analysis of failure data from accelerated stress conditions. In other words, reliability characteristics can be obtained in normal operating conditions using lifetime-stress model. Figure 1 presents the framework. Each phase of the framework will be described in the following.

A. Understanding The Stresses Affecting Product Failure

In order to investigate the failure process of any product, it is necessary to study the factors that directly affect its lifetime. In other words, if ALT is considered to accelerate the failure process of product, the type of stresses used in the test must also be specified. Any factor that directly reduces the lifetime of the product and its

variations are measurable could be used. These factors are often introduced by manufacturers. For example, in electrical system, factors such as temperature, voltage or electric current, and power fluctuations can reduce lifetime.

B. Determining The Number Of Stresses

Among the stresses that affect the lifetime of any product, one or more types of stresses can be considered to accelerate the failure process in ALT. The number of stresses is determined based on the type of product and the test conditions. Usually one type of stress is used in experiments when the lifetime of product is not too long. Also focusing on one type of stress makes performing the test easier compared to when two or more types of stress are used. Two or more types of stress can be used if the lifetime of product is long, which makes the experiment become more complex.

C. Determining The Stress Levels

Depending on the number of considered stresses, it is necessary to determine the levels of each stress variable, since in CSALT; the product could be exposed to several levels of one type of stress. The first level of stress is chosen to be a little more than the stress level in normal operating conditions, so that it decreases the lifetime of product. The next levels further reduce the lifetime of the product. The last level is chosen so that the product does not fail immediately.

D. Performing Accelerated Life Test

After determining the stresses and their levels, a certain number of products are selected as a sample for each level, and the test is then performed accordingly for a certain period or up to when a number of failures occur. The Observed failure times are recorded during the test.

E. Determining The Type Of Censoring Data

In order to reduce the test time and related costs, it is necessary to end the test at the specified time or after observing a number of failures for each stress level. Based on time or number of the failures, different types of censoring like left censoring, right censoring, interval censoring, random censoring, progressive censoring and Type-I and Type-II censoring can be considered for ALT. Likewise, by considering time and number of failures simultaneously, Type-I and Type-II hybrid censoring can be performed. Collecting information about both exact failure times and censored data is a fundamental task.

F. Data Analysis

After collecting the required data, statistical analysis of them begins. Statistical analysis consists of six steps which will be explained in the following.

Step 1. Choosing the lifetime distribution

When performing the reliability analysis, a distribution must be chosen to model the data. The more closely the distribution fits the data, the more likely the reliability statistics will accurately describe the performance of the product. The major distributions used in reliability analysis are: Exponential, Normal, Log-normal, Gamma, and Weibull. Using goodness of fit tests such as the Kolmogorov-Smirnov test and Anderson-Darling, the best distribution that fits the failure data is selected.

Step 2. Choosing the lifetime-stress model

Due to the changes in the shape or scale parameter of lifetime distribution in terms of the stress, a proper relationship between lifetime and stress is selected. Usually, when the stress level increases, less time is needed to reach the failure point, and when the stress level is reduced, the lifetime will increase. Different models are presented that describe the relationship between lifetime and stress, such as Arrhenius model [5], Eyring model, Inverse power law model, Log-Linear model and Proportional Hazards (Cox) model [42].

Step 3. Forming the likelihood function

The likelihood function is formed based on the type of sample observations (complete or censored) which is a function of the population parameters and observed samples. Here, the observations are known whereas the population parameters are unknown. Lifetime-stress relationship is also considered in the function. In general, suppose a random sample of size n is put into test, and $\mathbf{X}_1, \mathbf{X}_2, \dots, \mathbf{X}_n$ is the set of random failure times. Denote O as the set containing the indices which the failure times are observed; R as the set containing the indices which the failure times are right censored; L as the set containing the indices which the failure times are left censored; and I as the set containing the indices which the failure times are interval censored with the only knowledge that the real failure time \mathbf{x}_i is in the interval $[U_i, V_i]$. Then the likelihood (L) based on this sample is

$$L(\mathbf{x}_i, \theta) = \prod_{i \in O} f(\mathbf{x}_i; \theta) \prod_{i \in R} [1 - F(\mathbf{x}_i; \theta)] \quad (1)$$

$$\prod_{i \in L} F(\mathbf{x}_i; \theta) \prod_{i \in I} [F(V_i; \theta) - F(U_i; \theta)]$$

where θ is an unknown parameter, $i=1,2,\dots,n$, and $f(\mathbf{x}_i; \theta)$ and $F(\mathbf{x}_i; \theta)$ are probability density function

(PDF) and cumulative distribution function (CDF), respectively. Likelihood for other type of censoring can be constructed from following the same rationale.

Step 4. Maximum Likelihood Estimation

The method is based on the unknown population parameters. By optimizing the likelihood function based on parameters, the ones that are most consistent with the observed samples will be determined. In other words, the idea behind the maximum likelihood parameter estimation is to determine the parameter values that maximize the likelihood (or, equivalently, the log likelihood). In the case of censored data, other estimation methods such as least square method are less precise. Therefore, using MLE method in this case is considered to be more robust and results in estimators with good statistical properties. Usually, explicit expressions cannot be obtained through directly solving the likelihood equations. Instead, the numerical methods such as Newton-Raphson method or powerful tools in the analysis of incomplete data such as the Expectation-Maximization (EM) algorithm can be used. Fisher information matrix and consequently asymptotically variances of estimates are obtained directly from the numerical methods. The EM algorithm possesses several advantageous properties, such as stable convergence, compared to the Newton-Raphson method. So as a new approach, mathematical programming tools were used for estimating the maximum likelihood estimates of unknown parameters with mathematical solving approach. The general form of mathematical programming problem is

$$\text{Max } L \quad (2)$$

s.t

$$C_1 > 0 \quad (3)$$

$$C_2 < 0 \quad (4)$$

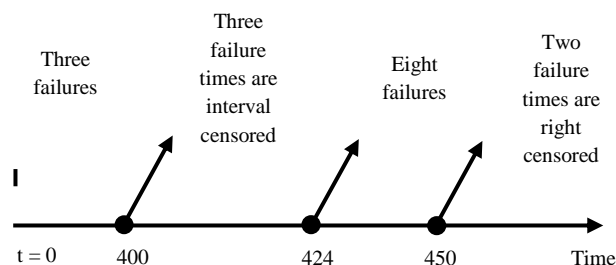


TABLE 1. COMPARISON OF PROPOSED MODEL WITH PRIOR MODELS.

Reference	Type of ALT	Type of censoring scheme	Lifetime distribution	Estimation features	Case study
Bai and Kim [18]	SSALT	Type-I	Weibull	MLE (Minimizing the asymptotic variance of the maximum likelihood estimator of a stated percentile at design stress.)	No
Xiong [19]	SSALT	Type-II	Exponential	MLE	No
Tang et al. [20]	CSALT	Type-I and Type-II	Exponential	The unbiased estimates were obtained for the parameters.	No
Abdel-Ghaly et al. [21]	SSALT	Type-I and Type-II	Weibull	MLE with a modified quasi-linearization method	No
Balakrishnan et al. [22]	SSALT	Type-II	Exponential	MLE for a cumulative exposure model	No
Balakrishnan and Xie [23]	SSALT	Type-I hybrid	Exponential	MLE for a cumulative exposure model	No
Li and Fard [24]	SSALT	Type-I	Weibull	MLE (Minimize the asymptotic variance of the maximum likelihood estimator of the life for a specified reliability)	No
Kateri and Balakrishnan [25]	SSALT	Type-II	Weibull	MLE with an iterative procedure in simplified estimator for initial estimates in the iterative process of MLE	No
Watkins and John [26]	CSALT	Type-II	Weibull	MLE	No
Abdel-Hamid and AL-Hussaini [27] Guan and Tang [28]	SSALT	Type-I	Exponential	MLE	No
Ling et al. [29]	SSALT	Type-I hybrid	Exponential	MLE minimizing the asymptotic variance of reliability estimate at a typical operating condition	No
Attia et al. [30]	CSALT	Type-I	Logistic	MLE	No
Lee and Pan [31]	SSALT	Type-II	Exponential	Bayesian Analysis	No
Wang et al. [32]	SSALT	Type-II	Geometric	MLE	Yes
Srivastava and Mittal [33]	CSALT	Type-I	Burr type-XII	MLE	No
Kamal and Zarrin [34]	CSALT	Type-I	Pareto	MLE	No
Aly and Bleed [35]	CSALT	Type-II	Logistic	Bayesian analysis	No
Shi et al. [36]	CSALT	Progressive Type-II Hybrid	Exponential	MLE and Bayes estimator	No
Aly and Bleed [37]	SSALT	Type-I	Logistic	MLE	No
Asser and Abd EL-Maseh [38]	CSALT	Type-I	Exponential	MLE	No
Amal et al. [39]	SSALT	progressively type-I interval	Weibull Poisson	MLE	No
Saleem [40]	SSALT	progressive type-I right	Weibull	Bayesian approach	No
Zhao et al. [41]	CSALT	Progressive Type-I Hybrid	Burr type-XII	MLE (The numerical method)	No
Proposed model	CSALT	Various types of censoring schemes	Weibull	MLE by a mathematical programming problem with meta-heuristic solution method	Yes

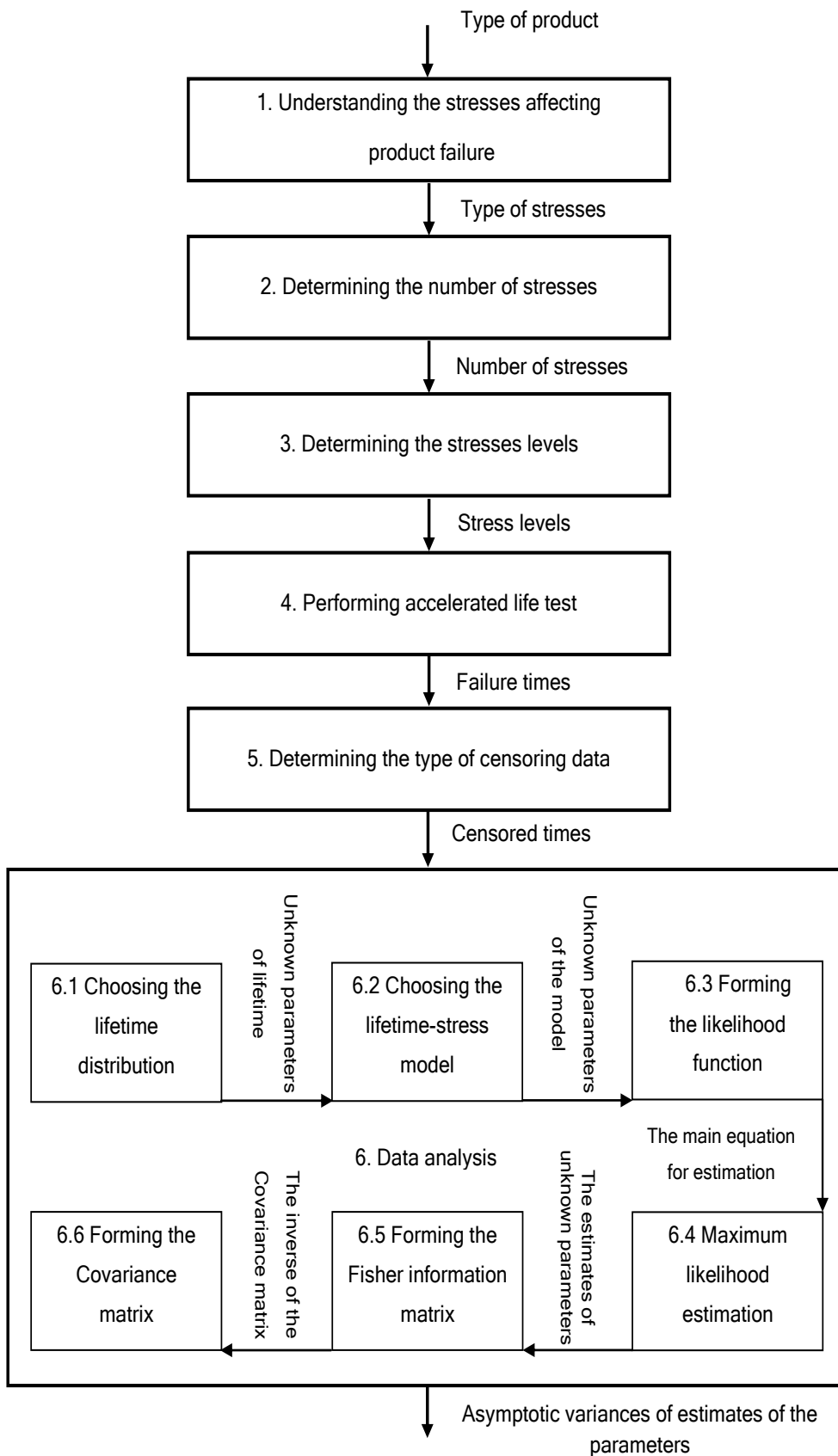


Fig. 1. The framework for Failure Process Modeling

As can be seen in (2), the objective of the mathematical programming problem was to obtain the maximum likelihood estimates of the unknown parameters which was derived by maximizing the likelihood function. The constraint (3) shows that the parameters of lifetime distribution should be positive. The constraint (4) indicates an inverse relationship between the lifetime and stress. The MLE of unknown parameters was obtained to maximize the likelihood function using optimization tools

Step 5. Forming the Fisher information matrix

The Fisher information matrix is a key tool in parameter estimation. It is a measure of the information content of the data relevant to the parameters being estimated. It is a symmetric matrix, the elements of which are the negative second partial and mixed partial derivations of of unknown parameters. Denote $\theta_1, \theta_2, \dots, \theta_n$ as the set of unknown parameters, then the Fisher information matrix is [5]

$$F = \begin{bmatrix} -\frac{\partial^2 \ln L}{\partial \theta_1^2} & -\frac{\partial^2 \ln L}{\partial \theta_1 \partial \theta_2} & \dots & -\frac{\partial^2 \ln L}{\partial \theta_1 \partial \theta_n} \\ -\frac{\partial^2 \ln L}{\partial \theta_2 \partial \theta_1} & -\frac{\partial^2 \ln L}{\partial \theta_2^2} & \dots & -\frac{\partial^2 \ln L}{\partial \theta_2 \partial \theta_n} \\ \vdots & \vdots & \ddots & \vdots \\ -\frac{\partial^2 \ln L}{\partial \theta_n \partial \theta_1} & -\frac{\partial^2 \ln L}{\partial \theta_n \partial \theta_2} & \dots & -\frac{\partial^2 \ln L}{\partial \theta_n^2} \end{bmatrix} \quad (5)$$

Step 6. Calculating the Covariance matrix

Covariance matrix is a symmetric matrix that shows the covariance between the variables. In general, estimation of Covariance matrix is asymptotic equals to the inverse of the Fisher information matrix and is given by [5]

$$\hat{\Sigma} = F^{-1} = \begin{bmatrix} \text{var}(\hat{\theta}_1) & \text{cov}(\hat{\theta}_1, \hat{\theta}_2) & \dots & \text{cov}(\hat{\theta}_1, \hat{\theta}_n) \\ \text{cov}(\hat{\theta}_2, \hat{\theta}_1) & \text{var}(\hat{\theta}_2) & \dots & \text{cov}(\hat{\theta}_2, \hat{\theta}_n) \\ \vdots & \vdots & \ddots & \vdots \\ \text{cov}(\hat{\theta}_n, \hat{\theta}_1) & \text{cov}(\hat{\theta}_n, \hat{\theta}_2) & \dots & \text{var}(\hat{\theta}_n) \end{bmatrix} \quad (6)$$

The variances all appear on the main diagonal of Covariance matrix. In other words, the purpose of calculating the Fisher information matrix is to obtain the asymptotic variance of the maximum likelihood estimates of the unknown parameters, the result of which is the confident intervals of the estimated parameters.

3. CASE STUDY

The object of this case study is the application of the framework in red LED lamps. An LED is a semiconductor light source. LEDs are used as indicator lamps in many devices and are increasingly used for other lighting applications such as aviation lighting, digital microscopes, automotive lighting, advertising, general lighting, and traffic signals. LEDs can have a relatively long useful life.

The six phases of framework from initial data collection to reliability parameter estimation will be described in the following.

A. Understanding The Stresses Affecting Led Lamps Failure

The definition of useful life is often given as the hours of operation during in which the LED’s output light has been decreased to 70% of initial output. The selection of 70% is based on vision research indicating that in general lighting applications, the typical human eye does not detect the decrease in light until it exceeds 30%. Optical and electrical parameters are critical in LED lamps. The input electric current and temperature cause stress in the LED crystalline structure. Also other factors such as power fluctuations, humidity, on and off frequency, and isolation affect the failure of LED lamps.

B. Determining The Number Of Stresses

Among the stresses mentioned in the previous phase, electric current, temperature, and humidity can be used because their levels could be increased. In this study, only electric current was investigated as the stress variable since a fixed electric current at a specified level is easier than fixing temperature or humidity at a specified level. By using the same experimental conditions, the effect of temperature and humidity was ignored.

C. Determining The Stress Levels

The stress level in the normal operating condition is five milliamper (mA). The stress levels of 20, 30 and 40 mA were selected. These stress levels were selected as follows: the first level (20 mA) was slightly greater than the level in the normal operating condition, and it resulted in reduction of the lifetime of the lamp. The second level (30 mA) reduced the lifetime of the lamp more quickly. The third level (40 mA) had the most effect in reduction of the lifetime of the lamp. Higher electrical current causes very fast failure and even melting of the lamp.

D. Performing Accelerated Life Test

Thirty four red LED lamps were tested at the room temperature. For stress level of 20 mA, 30 mA, and 40 mA, 16 lamps, 12 lamps, and six lamps were selected respectively.

E. Determining The Type Of Censoring Data

For stress level of 20 mA, the test was continued for 400 hours and failure times were recorded. For the period of 400 to 424 hours, no observation was performed. Then from 424 hours to 450 hours, observation was carried on and failure times were recorded. For stress level of 30 mA, the test was continued for 55 hours and failure times were recorded. For stress level of 40 mA, the test was continued for 30 hours and failure times were recorded. The type of censoring data used is represented as in Figures 2 to 4.

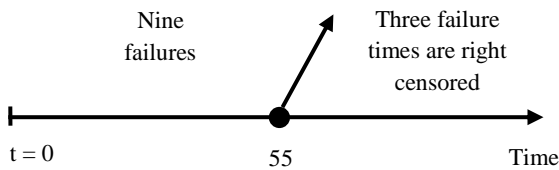


Fig 3. Schematic representation of censoring data under stress level of 30 milliamper.

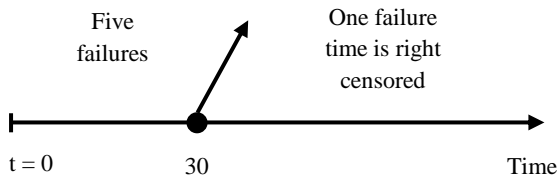


Fig 4. Schematic representation of censoring data under stress level of 40 milliamper.

So for stress level of 20 mA, the failure times of three lamps were interval censored while the failure times of two lamps were right censored. For stress level of 30 mA, the failure times of three lamps were right censored. For stress level of 40 mA, the failure time of one lamp was right censored. The observed failure times in three stress levels are listed in Table 2.

F. Data Analysis

Step 1. Choosing the lifetime distribution

The two-parameter Weibull distribution is widely used in reliability evaluation and analysis of lifetime data. Let us assume the lifetime random variable T follows the Weibull distribution with the shape and scale parameters of β and α , respectively. So the CDF and PDF of T are

$$F_T(t; \alpha, \beta) = 1 - e^{-\left(\frac{t}{\alpha}\right)^\beta} \tag{7}$$

and

$$f_T(t; \alpha, \beta) = \frac{\beta t^{\beta-1}}{\alpha^\beta} e^{-\left(\frac{t}{\alpha}\right)^\beta} \tag{8}$$

where

$$t > 0, \alpha > 0, \beta > 0.$$

TABLE 2. THE OBSERVED FAILURE TIMES IN THREE STRESS LEVELS.

Stress levels (mA)	Failure times
20	211 288 399 428 429 430 432 444 446 449 450
30	27 39 39 44 45 48 48 50 53
40	10 17 21 24 29

Step 2. Choosing the lifetime-stress model

In order to determine the best relationship between stress and Weibull distribution parameters, the parameters in each of the stress levels were estimated using Minitab software. These values are shown in Table 3.

TABLE 3. PARAMETERS OF WEIBULL DISTRIBUTION AT DIFFERENT STRESS LEVELS.

Stress levels(mA)	α	β
20	426.542	9.018
30	46.562	7.922
40	22.474	3.649

Considering the Linear relationship, Ln(power) relationship, Inverse power law relationship, and Arrhenius relationship between stress values and each of the parameters, the coefficient of determination (R^2) were calculated as reported in Table 4.

The Arrhenius relationship between the scale parameter and stress and the linear relationship between the shape parameter and stress were selected, because compared to the other relationships, their coefficients of determination are closer to one.

TABLE 4. R² VALUES REGARDING THE RELATIONSHIP BETWEEN THE PARAMETERS AND STRESS.

Relationships	α	β
Linear	0.794	0.896
Ln(power)	0.867	0.828
Inverse power law	0.966	0.780
Arrhenius	0.991	0.699

Therefore, the lifetime-stress models were obtained as follows:

$$\beta = A_1 + B_1 S \tag{9}$$

$$\alpha = A_2 e^{\frac{B_2}{S}} \tag{10}$$

where A_1, B_1, A_2 and B_2 are unknown parameters and S is the stress level.

Step 3. Forming the likelihood function

For forming the likelihood function, it is necessary to define a notation that is shown in Table 5.

Based on the interval and right censored data from Weibull distribution, the likelihood function under CSALT is given by:

$$\begin{aligned}
 &L(A_1, B_1, A_2, B_2) \\
 &= \prod_{i=1}^{n-d-c} f(t_i) \prod_{j=1}^d F(tR_j) - F(tL_j) \prod_{k=1}^c 1 - F(T_k) \\
 &= \prod_{i=1}^{n-d-c} \frac{A_1 + B_1 S_i}{\left(A_2 e^{\frac{B_2}{S_i}}\right)^{A_1 + B_1 S_i}} t_i^{A_1 + B_1 S_i - 1} e^{-\left(\frac{t_i}{A_2 e^{\frac{B_2}{S_i}}}\right)^{A_1}} \\
 &\quad \prod_{j=1}^d \left[e^{-\left(\frac{tL_j}{A_2 e^{\frac{B_2}{S_j}}}\right)^{A_1 + B_1 S_j}} - e^{-\left(\frac{tR_j}{A_2 e^{\frac{B_2}{S_j}}}\right)^{A_1 + B_1 S_j}} \right] \\
 &\quad \prod_{k=1}^c e^{-\left(\frac{T_k}{A_2 e^{\frac{B_2}{S_k}}}\right)^{A_1 + B_1 S_k}}
 \end{aligned} \tag{11}$$

TABLE 5. LIST OF NOTATIONS.

Notation	Definition
t_i	Observed failure time of unit i
S_i	The stress applied to unit i at time t_i
S_j	The stress applied to unit j upon failure
S_k	The stress applied to unit k upon failure
tL_j	The lower bound of the time interval in which unit j fails
tR_j	The upper bound of the time interval in which unit j fails
T_k	The lower bound of the time interval in which unit k fails
n	Sample size (total number of test units in CSALT)
d	The number of units that fail in the time interval $[tL_j, tR_j]$ (interval censored observations)
c	The number of units that fail in the time interval $[T_k, +\infty]$ (right censored observations)
$n-d-c$	The number of units for which the exact failure times are observed (complete observations)

Using $\ln L$ to denote the natural logarithm of $L(A_1, B_1, A_2, B_2)$, then we have

Step 4. Maximum Likelihood Estimation

In this case study, the estimation of parameters was considered under CSALT with interval censored and right censored data assuming two-parameter Weibull lifetime distribution. After equating the first partial derivatives of $\ln L$ with respect to A_1, B_1, A_2 and B_2 to zero and substituting the numerical values in the equations, it was observed that due to complex and nonlinear equations, getting closed form of estimates of the unknown parameter was not possible. So, as a new approach, mathematical programming tools were used for estimating these parameters with the mathematical solving approach.

$$\begin{aligned}
 &\ln L(A_1, B_1, A_2, B_2) \\
 &= \sum_{i=1}^{n-d-c} \ln(A_1 + B_1 S_i) \\
 &\quad + (A_1 + B_1 S_i - 1) \ln(t_i) \\
 &\quad - t_i^{A_1 + B_1 S_i} (A_2 e^{\frac{B_2}{S_i}})^{-A_1 - B_1 S_i} - (A_1 + B_1 S_i) \left(\ln(A_2) + \frac{B_2}{S_i} \right) \\
 &\quad + \sum_{j=1}^d \ln \left(e^{-tL_j^{A_1 + B_1 S_j} (A_2 e^{\frac{B_2}{S_j}})^{-A_1 - B_1 S_j}} - e^{-tR_j^{A_1 + B_1 S_j} (A_2 e^{\frac{B_2}{S_j}})^{-A_1 - B_1 S_j}} \right) \\
 &\quad + \sum_{k=1}^c -T_k^{A_1 + B_1 S_k} (A_2 e^{\frac{B_2}{S_k}})^{-A_1 - B_1 S_k}
 \end{aligned} \tag{12}$$

The mathematical programming problem is

$$\text{Max } \ln L(A_1, B_1, A_2, B_2) \tag{13}$$

s. t

$$A_1 + 40B_1 \geq 0 \tag{14}$$

$$A_2 \geq 0 \tag{15}$$

$$B_1 \leq 0 \tag{16}$$

$$B_2 \geq 0 \tag{17}$$

As can be seen in (13), the objective of the mathematical programming problem was to obtain the maximum likelihood estimates of the unknown parameters A_1, B_1, A_2 and B_2 which was derived by maximizing $\ln L$. The inequality (14) shows the positive lifetime constraint. In other words, even at the highest stress level (40 mA), negative lifetime should not be observed, and the shape parameter of Weibull distribution should be positive. The inequality (15) also shows that the scale parameter of Weibull distribution should be positive. The Inequalities (16) and (17) indicate an inverse relationship between shape parameter and scale parameter of lifetime distribution and stress respectively.

Considering this case as a minimization problem, since the logarithm of likelihood function was not convex, the optimization toolbox of Matlab software was unable to find the global optimum solution. Due to the nonlinear programming problem, meta-heuristic algorithms could be used to solve the problem. Among the meta-heuristic algorithms, GA has accuracy and requires less time in solving problems. Likewise, this algorithm has more capability and is easier to model. Therefore, based on the predictability and convergence of genetic algorithm, GA toolbox was used to solve the problem.

GA became popular through the work of Holland in the early 1970s, particularly his book "Adaptation in Natural and Artificial Systems" [43]. GA is a search heuristic that mimics the process of natural selection and is routinely used to generate useful solutions to optimization and search problems.

The evolution usually starts from a population of randomly generated individuals, and is an iterative process, with the population in each iteration called a generation. In each generation, the fitness of every individual in the population is evaluated; the fitness is usually the value of the objective function in the optimization problem being solved. The more fit individuals are stochastically selected from the current population, and each individual's genome is modified (recombined and possibly randomly mutated) to form a new generation. The new generation of candidate solutions is then used in the next iteration of the algorithm. Commonly, the algorithm is terminated when either a maximum number of generations has been produced, or a satisfactory fitness level has been reached for the population.

After 160 iterations, the GA is converged to the optimum solution as follows:

$$\hat{A}_1 = 0.183 \quad (18)$$

$$\hat{B}_1 = -0.001 \quad (19)$$

$$\hat{A}_2 = 16.105 \quad (20)$$

$$\hat{B}_2 = 5.067 \quad (21)$$

$$\ln L = 219.289 \quad (22)$$

The convergence graph of GA is shown in Figure 5.

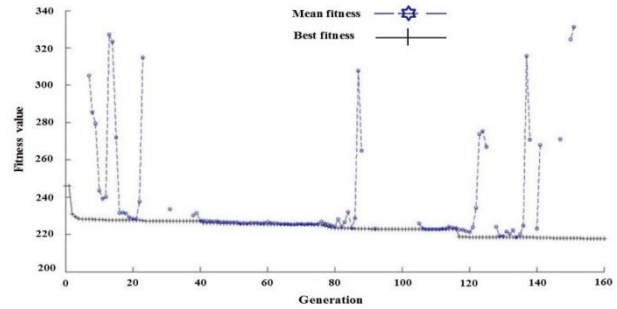


Fig 5. The convergence graph of genetic algorithm.

Step 5. Forming the Fisher information matrix

In order to form the Fisher information matrix, the second order partial and mixed partial derivations of the log likelihood function were calculated with respect to A_1 , B_1 , A_2 and B_2 . By substituting the numerical values consisting of the MLE of parameters, stress levels, the observed failure times and censored times, the Fisher information matrix was obtained as follows:

$$F = \quad (23)$$

$$= \begin{bmatrix} \frac{-\partial^2 \ln L(A_1, B_1, A_2, B_2)}{\partial A_1^2} & \frac{-\partial^2 \ln L(A_1, B_1, A_2, B_2)}{\partial A_1 \partial B_1} & \frac{-\partial^2 \ln L(A_1, B_1, A_2, B_2)}{\partial A_1 \partial A_2} & \frac{-\partial^2 \ln L(A_1, B_1, A_2, B_2)}{\partial A_1 \partial B_2} \\ \frac{-\partial^2 \ln L(A_1, B_1, A_2, B_2)}{\partial B_1 \partial A_1} & \frac{-\partial^2 \ln L(A_1, B_1, A_2, B_2)}{\partial B_1^2} & \frac{-\partial^2 \ln L(A_1, B_1, A_2, B_2)}{\partial B_1 \partial A_2} & \frac{-\partial^2 \ln L(A_1, B_1, A_2, B_2)}{\partial B_1 \partial B_2} \\ \frac{-\partial^2 \ln L(A_1, B_1, A_2, B_2)}{\partial A_2 \partial A_1} & \frac{-\partial^2 \ln L(A_1, B_1, A_2, B_2)}{\partial A_2 \partial B_1} & \frac{-\partial^2 \ln L(A_1, B_1, A_2, B_2)}{\partial A_2^2} & \frac{-\partial^2 \ln L(A_1, B_1, A_2, B_2)}{\partial A_2 \partial B_2} \\ \frac{-\partial^2 \ln L(A_1, B_1, A_2, B_2)}{\partial B_2 \partial A_1} & \frac{-\partial^2 \ln L(A_1, B_1, A_2, B_2)}{\partial B_2 \partial B_1} & \frac{-\partial^2 \ln L(A_1, B_1, A_2, B_2)}{\partial B_2 \partial A_2} & \frac{-\partial^2 \ln L(A_1, B_1, A_2, B_2)}{\partial B_2^2} \end{bmatrix} = \begin{bmatrix} 1397.874 & 36822.168 & -2.006 & -1.476 \\ 36822.168 & 1051471.328 & -45.730 & -32.314 \\ -2.006 & -45.730 & 0.0153 & 0.003 \\ -1.476 & -32.314 & 0.003 & 0.002 \end{bmatrix}$$

Step 6. Forming the Covariance matrix

The asymptotic Covariance matrix Σ of the maximum likelihood estimates \hat{A}_1 , \hat{B}_1 , \hat{A}_2 and \hat{B}_2 was obtained by inverting the Fisher information matrix F for the large sample size. So the Covariance matrix was obtained as follows

$$\hat{\Sigma} = F^{-1} = \begin{bmatrix} \text{var}(\hat{A}_1) & \text{cov}(\hat{A}_1, \hat{B}_1) & \text{cov}(\hat{A}_1, \hat{A}_2) & \text{cov}(\hat{A}_1, \hat{B}_2) \\ \text{cov}(\hat{B}_1, \hat{A}_1) & \text{var}(\hat{B}_1) & \text{cov}(\hat{B}_1, \hat{A}_2) & \text{cov}(\hat{B}_1, \hat{B}_2) \\ \text{cov}(\hat{A}_2, \hat{A}_1) & \text{cov}(\hat{A}_2, \hat{B}_1) & \text{var}(\hat{A}_2) & \text{cov}(\hat{A}_2, \hat{B}_2) \\ \text{cov}(\hat{B}_2, \hat{A}_1) & \text{cov}(\hat{B}_2, \hat{B}_1) & \text{cov}(\hat{B}_2, \hat{A}_2) & \text{var}(\hat{B}_2) \end{bmatrix} = \quad (24)$$

$$\begin{bmatrix} 0.1533 & -0.0040 & -0.9008 & 46.4559 \\ -0.0040 & 0.0001 & 0.0235 & -1.1799 \\ -0.9008 & 0.0235 & 95.2362 & -395.9830 \\ 46.4559 & -1.1799 & -395.9830 & 15104.7969 \end{bmatrix}$$

The approximate $(1-\alpha)$ 100% confidence intervals for A_1 , B_1 , A_2 and B_2 are given by [44]

$$\hat{A}_1 \pm Z_{\alpha/2} \sqrt{\text{var}(\hat{A}_1)}, \hat{B}_1 \pm Z_{\alpha/2} \sqrt{\text{var}(\hat{B}_1)}, \\ \hat{A}_2 \pm Z_{\alpha/2} \sqrt{\text{var}(\hat{A}_2)},$$

$$\widehat{B}_2 \pm Z_{\alpha/2} \sqrt{\text{var}(\widehat{B}_2)} \quad (25)$$

where $Z_{\alpha/2}$ is the $100(1-\alpha/2)$ percentile of a standard normal variate. The 95% confidence intervals A_1, B_1, A_2 and B_2 are presented in Table 6.

TABLE 6. THE 95% CONFIDENCE INTERVALS OF PARAMETERS.

Parameters	95% lower limit	95% upper limit
$\widehat{A}_1 = 0.183$	-0.583	0.949
$\widehat{B}_1 = -0.001$	-0.0206	0.0186
$\widehat{A}_2 = 16.105$	-3.0224	35.2324
$\widehat{B}_2 = 5.067$	-235.8199	245.9539

According to the estimates obtained for the parameters A_1, B_1, A_2 and B_2 , the shape and scale parameters of the Weibull distribution in stress level of 5 mA (normal operating conditions) can be obtained from equations (9) and (10) as follows:

$$\widehat{\beta} = 0.178 \quad (26)$$

$$\widehat{\alpha} = 44.3685 \quad (27)$$

Reliability function of two-parameter Weibull distribution (which has been plotted in Figure 6) for a specified period of time t can be directly derived by using the estimated parameters from equations (26) and (27) as follows:

$$R(t) = e^{-\left(\frac{t}{44.3685}\right)^{0.178}} \quad (28)$$

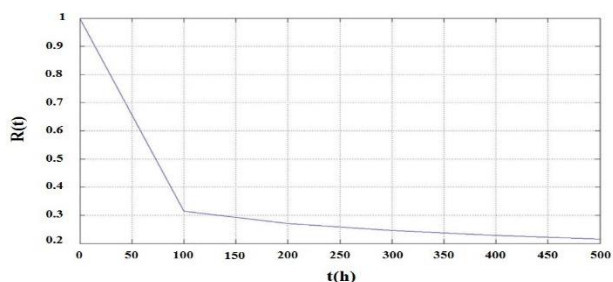


Fig. 6. Reliability function at different service times in normal operating condition.

The main percentiles of lifetime distribution were calculated according to the reliability function as shown in Table 7.

TABLE 7. PERCENTILES OF LIFETIME DISTRIBUTION.

Percentiles	Lifetime
10 th	0.464
25 th	0.405
50 th	0.360
75 th	0.333
90 th	0.322
95 th	0.318

4. CONCLUSION

In this paper, we have presented a framework defining a new approach for FPM with censored data in CSALTs. The FPM plays a key role in the reliability analysis of systems. Therefore, a correct definition of the model describing the failure process is a very important issue that has been less focused on. In addition, in the previous studies, up to three types of censoring schemes have been investigated, whereas the various types of censoring schemes have been considered for the first time in this study.

A case study was developed in red LED lamps. CSALT with three stress levels under interval censored and right censored data was applied. After forming the likelihood function, it was observed that the maximum likelihood estimates could not be obtained in the closed form. Numerical methods such as Newton-Raphson method can be used to compute them. The Newton-Raphson method is a direct approach for estimating the relevant parameters in a likelihood function, which uses the observed information matrix. When censoring is used, the observed information matrix shows more variability, especially when the sample size is small. In this paper, as a new approach, mathematical programming with a mathematical solving approach was proposed and used as a tool to compute the maximum likelihood estimates. The maximum likelihood estimates of unknown parameters were obtained using GA. The Results obtained for the Covariance matrix show that some asymptotic variances of estimates of the parameters were great. In general, the estimates obtained from the censored data have less accuracy compared to the complete data. In other words, the greater the amount of censored data, the less the convergence of estimates of the parameters to the true value is, and thus, the asymptotic variance increases. The precision of estimation will be improved by increasing the sample size.

In fact, the precision of estimates of the parameters depends on the test design (sample size, test time, number of failures, etc.). Similarly, since the reducing test time and related costs are some of the main reasons for censoring

data, there should be a balance between test time, sample size and results performance of statistical inference of test.

Finally, as a future work, in order to increase the precision of estimation, optimization criteria such as minimization of asymptotic variance of estimates of the reliability parameters can be considered and the optimum model can be designed accordingly. The optimal design of CSALTs can be studied to specify the optimal sample size and censoring times. Additionally, using powerful tools in the analysis of censored data such as the Expectation–Maximization algorithm is proposed for estimating the parameters.

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